NASA TH X- 55587

AN ATLAS OF STRATOSPHERIC MEAN ISOTHERMS DERIVED FROM TIROS VII OBSERVATIONS

ORM 602	N67-11365	(THRU)
FACILITY F	(PAGES) TM X - 5 5 5 8 7 (NASA CR OR TMX OR AD NUMBER)	(CODE)

I GPO PRICE &	BY -
GPO PRICE \$	JAMES S. KENNEDY
CFSTI PRICE(S) \$	CAPTAIN, USAF
Hard copy (HC)	
Microfiche (MF)	
ff 653 July 65	

JULY 1966



GODDARD SPACE FLIGHT CENTER GREENBELT, MD.

AN ATLAS OF STRATOSPHERIC MEAN ISOTHERMS DERIVED FROM TIROS VII OBSERVATIONS

James S. Kennedy*
Captain, USAF

GODDARD SPACE FLIGHT CENTER Greenbelt, Maryland

^{*}Air Weather Service member temporarily attached to Goddard Space Flight Center.

N67-11365

ABSTRACT

The TIROS VII Meteorological Satellite, launched 19 June 1963, was equipped with a medium resolution scanning radiometer. One of the spectral regions observed, the 15 micron region, largely measured the emission from the stratosphere. The spatial and temporal variations of the observed 15 micron emission were found to correspond closely to major thermal patterns of the stratosphere. The data have been compiled and mapped on a series of ten-day mean charts, normally at five-day intervals, covering the 13-month period subsequent to launch. The charts comprise data from regions of the globe normally inaccessible to conventional means and are presented as a guide to stratospheric behavior during the period of June 1963 to July 1964. aukon

CONTENTS

																							$\frac{\text{Page}}{}$
1.	INTRO	DUCTION .			•						•			•	•		•	•		•			1
2.	15 MIC	RON RADIOMI	ETER				•	•	•	•	•	•	•		•	•	•	•	•	•	•	•	2
3.	DATA	DEFICIENCES	S	•	•	•					•	•		•	•	•	•	•	•	•	•	•	4
	3.2 S	Degradation . Signal-To-Noise Seographic Loc	Ratio	0	•	•	•	•	•	•	•	•	•		•		•	•	•	•		•	4 5 5
	3.4 I	ata Coverage		•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	6
4.	MAPP	ING PROCEDU	RES				•	•	•	•							•					•	6
5.	TEN-I	OAY MEAN CH	ARTS	•			•		•				•	•	•		•	•		•	•		9
ACK	NOWL	EDGEMENTS				•			•				•	•	•	•	•	•	•	•	•	•	10
REF	EREN	CES · · · ·		•	•	•	•	•		•	•	•	•	•	•	•	•	•	•	•	•	•	12
CHA	RTS .			•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	13-85
			LIST	ГΟ	F	II	LU	JS'	ΤF	RΑ	ΤI	ON	ıs										
Figu	ıre																						
1	(a)	Typical temper ments to the 'North summer 15° North	U.S.	Sta	anc	laı	d	Αt	m	os	ph	er	e]	196	321	¹ f	\mathbf{or}	60)°	-			
	(b)	Weighting functions going radiance								g t	o t	he	n	ıea	ısı	ıre	ed	ou	ıt-				
	(c)	Weighting fundoutgoing radia			-							th	e .	me	eas •	su:	rec	d •		•	•		3
2		plitude respona ridional and zo																				•	9
Tab	<u>le</u>		I	JIS'	Г	OI	? <u>'</u>	ΤА	. B .	LE	S												
I	Do	cumentation Da	ita Co	nce	er	nir	ıg	15	M	lic	ro	n (Ch	ar	ts		•	•	•		•		11

AN ATLAS OF STRATOSPHERIC MEAN ISOTHERMS DERIVED FROM TIROS VII OBSERVATIONS

1. INTRODUCTION

The TIROS VII weather satellite, launched 19 June 1963, included a five-channel scanning radiometer among its complement of meteorological sensors. One of the radiometric channels was sensitive in the 15 micron spectral region where atmospheric emission is predominately due to the 15 micron vibration-rotation band of carbon dioxide. The primary goal of the 15 micron experiment was to examine the suitability of the spectral region for horizon sensing (Bandeen et al., 1963). The advantages inherent in the 15 micron region are: (1) the very short unit optical depths of the troposphere minimize the effect of tropospheric phenomena, specifically clouds, on the outgoing emission, and (2) carbon dioxide is the only major absorber in the 5 to 30 micron region, the region which encompasses the bulk of atmospheric emission, which is present in sensibly constant mixing ratios at altitudes of significant emission.

Implicit in the aforementioned properties of the 15 micron region is the fact that variations in observed emission are due primarily to horizontal variations in the temperature field at levels of significant emission. It will be shown that most of the emission reaching the satellite originates in the stratosphere. Thus a mapping of observed emission duplicates, to a large extent, the major thermal patterns of the stratosphere.

While the extension of in situ measurements of upper atmosphere parameters, especially since the International Geophysical Year of 1957, has been accelerated, large areas of sparse data exist even in the Northern Hemisphere. The Southern Hemisphere, except for localized areas, is a major data gap. Therefore, we feel that even relatively unconventional means such as the remote measurements by the 15 micron channel of TIROS VII, should be studied to the fullest extent to explore the behavior of hitherto forbidden areas. To quote Prof. V.P. Starr, ". . . many new conceptions concerning the operation of the atmosphere are to be looked for at the borderline of measurability" (Starr and Wallace, 1964).

The TIROS VII 15 micron data have been compiled into a series of ten-day, global mean-temperature charts covering a period of 13 months. The following sections will examine in more detail the physical significance of the 15 micron sensor and describe the manner in which the charts were constructed.

2. 15 MICRON RADIOMETER

The 15 micron channel of the five-channel scanning radiometer was sensitive from 14.8 to 15.5 microns. The field of view of the instrument was five degrees between the half-power points. From the mean satellite altitude of 635 km, the minimum instantaneous area viewed as projected on the earth was about 2400 sqkm when the optical axis was normal to the surface.

The optical axis of the radiometer was at a fixed angle of 45 degrees from the spin axis of the satellite. The radiometer viewed in two colinear directions, 180 degrees apart, known as floor side and wall side. At least one side was exposed to outer space at all times, providing a check point of absolute zero. The spinning motion of the satellite at the rate of about 10 rpm, combined with the orbital motion with the spin axis approximately fixed with respect to inertial space, produced a rather complicated pattern of scanning (Allison and Warnecke, 1964; also Staff Members, 1964, Vol. 1, App. B). The orbital inclination of the spacecraft was 58.2 degrees, prohibiting observations poleward of about 60 degrees latitude.

A detailed description of the components of the radiometer and its method of operation is contained in the <u>TIROS VII Radiation Data Catalog and Users' Manual</u> (Staff Members, 1964). The emphasis here is on the relation of the measurements to stratospheric temperatures.

It is possible to decompose the total outgoing radiation into contributions as a function of altitude based on the radiative properties of carbon dioxide and the spectral response of the radiometer (Nordberg et al., 1965). Figure 1 shows the results for four model atmospheres and two extremes of nadir angle. ψ (h) expresses the weight given to various altitudes.

While the weighting curves are rather blunt and broad, it may be seen that most of the outgoing energy originates in the region from 10 to 35 km. The absolute maxima at low nadir angles is at about 23-25 km which corresponds to roughly a pressure of 25-35 mb. Figure 1(c) shows that the weighting functions shift upward somewhat at larger nadir angles. To reduce the dependence of the observations on nadir angle, only measurements made with nadir angles of 40 degrees or less were used in this study.

At low nadir angles, more than 96 percent of the total outgoing intensity originates at levels above 10 km. Cloudiness, therefore, does not greatly affect the observed energy. The effect of cloudiness would be the greatest for a tropical atmosphere at zero degree nadir angle, due to the high tropopause and large difference between surface and tropopause temperature. Since the Tropics is a

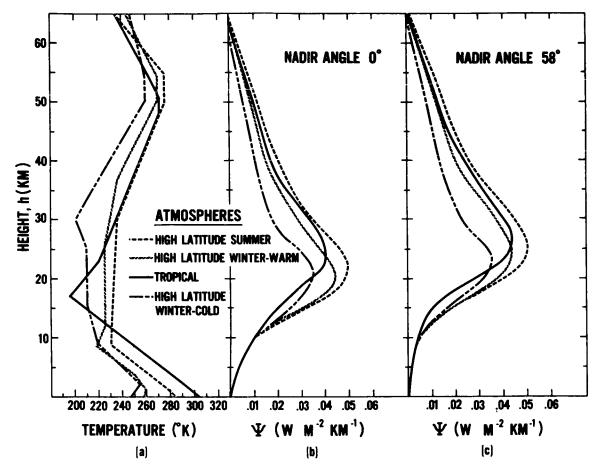


Figure 1. (a) Typical temperature profiles based on proposed supplements to the "U.S. Standard Atmosphere 1962" for 60° North summer, 60° North winter (warm and cold) and 15° North (b) Weighting functions $\psi(h)$, applying to the measured outgoing radiance; nadir angle = 0° (c) Weighting functions, $\psi(h)$, applying to the measured outgoing radiance; nadir angle = 58°

region of persistent high cloudiness, the effect of clouds was calculated from radiative transfer theory to obtain a limiting "worst case" (Kunde, 1966). The result was found to be that an overcast at the tropopause would reduce the derived mean temperature by only three degrees Kelvin as compared with clear skies. At higher latitudes, the effect is much less. Due to the very weak horizontal temperature gradients in the tropical stratosphere, cold pockets associated with areas of persistent high cloudiness are frequently found. The lower readings may be partially due to actual colder stratospheric temperatures caused by cloudy insulation of the stratosphere from tropospheric heat sources.

The observations at higher latitudes are more physically meaningful in the context of stratospheric dynamics partly because the effect of cloudiness is nil

but more importantly, because the lapse rates from 10 to 30 km are nearly isothermal as shown in Figure 1(a). Weighted mean temperature patterns at high latitudes will correspond more nearly to true temperature patterns at a given level than in the Tropics where there is a sharp discontinuity at the tropopause. An added complication in the Tropics is the double reversal of the horizontal poleward temperature gradient from troposphere to lower stratosphere and from lower stratosphere to mid-stratosphere.

The energy received by the radiometer was converted into units of equivalent blackbody temperature (T_{BB}). Equivalent blackbody temperature is defined as the temperature of an isothermal blackbody filling the field of view (as in the laboratory calibration) which would cause the same response from the radiometer as does the generally non-Planckian spectral distribution of the radiation emerging from the top of the atmosphere in the direction of the satellite. Since a vertically-weighted-mean temperature does not easily fit into the framework of existing conventional measurements, we feel that the global patterns produced from 15 micron data are much more meaningful than the absolute values of equivalent blackbody temperature. The next section describes the manner in which the 15 micron data are displayed.

3. DATA DEFICIENCIES

While knowledge of stratospheric behavior from existing conventional measurements was the prime consideration in the format of the data, modifications and compromise were necessitated by the following factors: (1) progressive degradation of the radiometer, (2) low signal-to-noise ratio of the radiometer, (3) errors in geographically locating the data, (4) gaps in global coverage.

3.1 Degradation

The radiometer did not have onboard calibration except for a zero degree reference when viewing outer space. The performance of the instrument was checked by computing mean quasi-global temperatures as a function of time. (The quasi-globe is that portion of the earth viewed by TIROS VII, roughly 65 N to 65 S latitude.) It was found that the mean temperatures decreased sharply during the first 30 days after launch and decreased at a much slower rate thereafter. The cause is unknown. In addition, the wall side and floor side recorded different readings for the same target viewed a few minutes apart. The difference between wall and floor side measurements increased with time and was also found to be a function of the temperature of the viewed region. Corrections were determined by fitting smooth curves through the global mean wall and floor side temperatures and correcting back to temperatures shortly after launch. A

detailed description of the degradation is contained in the TIROS VII manual (Staff Members, 1964). Briefly each measurement was modified by applying a correction, ΔT , in the form,

$$\Delta T_{f,w}(t) = a_{f,w}(t) + b_{f,w}(t)T_{f,w}$$
 (1)

where

f = Floor Measurement
 w = Wall Measurement
 a, b = Correction Factors

t = Time

T = Uncorrected Observed Temperature

The correction factors, a and b, were determined from degradation nomograms in the TIROS VII manual (Staff Members, 1965, Vol. 3). The time scale of the degradation was sufficiently slow that the factors could be computed for the mid-date of any map and used for all data included in the map, usually that observed over a 10-day period. The degradation of the instrument casts some doubt on the validity of the absolute value of the measurements but does not greatly affect the final temperature patterns.

3.2 Signal-To-Noise Ratio

The 15 micron channel measurements were characterized by a random noise component with an rms amplitude of about 5 degrees Kelvin. The noise component was largely eliminated by time and spatial averaging which will be described later.

3.3 Geographic Location

Depending on the angle between the spin axis and local vertical, the radiometer scans the earth in one of three distinctive patterns (Allison and Warnecke, 1964). When the spin axis is nearly vertical, the radiometer traces a helical pattern on the ground which does not cross the horizon, known as closed mode. When the spin axis is nearly horizontal, the radiometer scans the earth alternately from floor and wall sides, known as the alternating open mode. At intermediate angles, which constitute the major portion of the total data, the radiometer describes a series of open arcs, all traced by either the floor or wall side, known as the single open mode.

In the single open mode the horizon is traversed twice during each rotation of the satellite, and the known length and time of the scan enable the data to be precisely located. In the closed mode, the spin rate of the spacecraft must be interpolated from the single open mode data measured just prior and subsequent to the closed mode. Since the spin rate varies somewhat due to magnetic torques

and other factors, the data are subject to misplacement. In the alternating open mode, the computer distinguishes between the alternate floor and wall side measurements by the respective lengths of the earth-viewed portion of the scans. Midway through the alternating mode sequence, the floor and wall scans are approximately equal and the computer is apt to mislabel the scans, resulting in a gross mislocation of data.

As mentioned in a previous section, the computer was instructed to reject all data with nadir angles greater than 40 degrees to minimize changes in the weighting curves. To avoid mislocation of data, a proviso was added that all scans with minimum nadir angles occurring within the scan greater than 38 degrees be rejected completely. All ambiguous portions of the alternating mode cycle were thus eliminated as well as most of the closed mode.

3.4 Data Coverage

The orbital inclination of the satellite, 58.2 degrees, prohibited measurements poleward of approximately 60 degrees latitude. Limitations in acquiring the data from the spacecraft resulted in additional gaps within the confines of the quasi-globe. Of the nearly 15 orbits per day experienced by TIROS VII, a maximum of nine orbits can be interrogated by the three Command and Data Acquisition stations in North America during any given interrogation day. The interrogation day includes all orbits interrogated in the series of nine consecutive orbits which come within range of the acquisition stations during each 24-hour period. The interrogation day often occurs on two seperate calendar days. The orbits acquired on one interrogation day are compiled on one Final Meteorological Radiation Tape (FMRT).

Two regions of the quasi-globe are never viewed, Central Siberia and southern South America. On most days, less than the optimum nine orbits are acquired. In the latter half of the 13 months of mapped 15 micron data, rarely are more than four orbits acquired per interrogation day. To fill out the quasi-globe and also to overcome random noise, several FMRT's, usually ten, were combined to produce one map. The rationale for ten-day maps will be covered in the next section.

4. MAPPING PROCEDURES

While grouping and altering the 15 micron data were necessitated by technical deficiencies as outlined in the previous section, ultimately, the characteristic spatial and time scales of the major stratospheris phenomena must be considered to arrive at a meteorologically useful product. In brief, the stratosphere

above 20 km is characterized by large scale, slow moving disturbances superimposed on a zonal current. Teweles (1963) has shown that most of the eddy activity is explained by zonal wave numbers one through four. Boville (1960), using 25 mb temperature data from Resolute, N.W.T., performed a spectral analysis and found that most of the variance is found in the seasonal shift of temperature, with a secondary maximum in the 16 to 32 day range associated with baroclinic waves. The findings of these authors guided the choice of length and time parameters.

A Mercator map base was selected for the data display as being most suitable for the quasi-globe. The data were gathered on a rectangular grid of equispaced points, each grid point being assigned the average value of all observations falling within its square of influence. The spacing of grid points was constant at five degrees of longitude in the zonal direction and variable, ranging from five degrees of latitude at the equator to about 2.5 degrees at latitude 60 degrees, in the meridional direction. The zonal grid spacing permits the resolution of disturbances up to wave number 36; however, spatial filtering was employed to filter such high wave numbers.

The long time scale of stratospheric phenomena enabled us to compile the data into ten-day mean charts at five-day intervals. Actually, the FMRT, rather than the calendar, was our basic time unit and the charts comprise 9 to 11 FMRT's depending on circumstances. During the course of the 13 months of observation, there were days or groups of days when no data were recorded. The FMRT's included in a chart were then either expanded or contracted to avoid overlapping such periods. The days of no data also prohibited the maintenance of a constant five day interval between charts throughout the 13 months. The term mean chart is somewhat of a misnomer. Certain areas of the quasi-globe may have been sampled once, daily, or not at all during the period of a chart. Slow moving stratospheric disturbances and strong spatial smoothing are the two factors which mitigated the random sampling of data.

The use of about ten days of data helped to overcome two of the major data deficiencies: data gaps and random noise. Throughout much of the 13 months of observation, a ten-day period comprises 50 to 70 orbits, and even during data-poor periods, 20 to 30 orbits. The average temperature at an individual grid point usually comprised hundreds, often thousands of observations.

After the data had been gathered on the grid array, two factors were dealt with before analysis could begin. First, all grid points of the quasi-globe did not have an assigned temperature. Any average temperature comprising less than 40 observations was rejected because of random noise. Since an electronic curve plotter was used for analysis, a complete field of data was required. The

grid array was completed by linear interpolation across data gaps in a zonal direction. This method approximates the technique a human analyst would employ.

Second, the temperature field contained many short wave perturbations which were considered to be noise. Partially, the perturbations were due to the quantization of mean temperatures into integer values by the computer. An electronic curve plotter cannot selectively ignore such minor variations and therefore the temperature was smoothed by a two dimensional spatial filter.

The filter was designed to leave the longest wavelengths unchanged in amplitude and phase and eliminate the shortest wavelengths. The filter was constructed following the method of Wallington (1962).

Basically, two different filters each having three weights in the meridional direction and nine weights in the zonal direction were passed over the grid array and the weighted temperature was assigned to the central value. The same result could have been derived in one step using a five-by-seventeen filter but would have had to be modified when the operator included external grid points. Using two three-by-nine filters in succession resulted in the loss of only the northernmost and southernmost line of data. Since the data are cyclic with period 2π in the zonal direction, the array was equivalent to a hollow cylinder with only the top and bottom lines of data being external points.

The first filter had a weight array as follows:

0.002 0.004 0.002	-0.043 -0.086 -0.043	0.354 0.708 0.354	-1.358 -2.716 -1.358	2.342 4.684 2.342	-1.358 -2.716 -1.358	0.354 0.708 0.354	-0.043 -0.086 -0.043	0.002 0.004 0.002
The sec	cond filter	was,						
0.002 0.004	$\begin{array}{c} 0.012 \\ 0.024 \end{array}$	$\begin{matrix}0.031\\0.062\end{matrix}$	$\begin{matrix} 0.051 \\ 0.102 \end{matrix}$	$\begin{matrix}0.058\\0.116\end{matrix}$	$\begin{matrix}0.051\\0.102\end{matrix}$	0.031 0.062	$\begin{array}{c} 0.012 \\ 0.024 \end{array}$	$\begin{matrix} 0.002 \\ 0.004 \end{matrix}$
0.002	0.012	0.031	0.051	0.058	0.051	0.031	0.012	0.002

Both filters are symmetrical in the meridional and zonal directions to eliminate any phase shift of the filtered harmonics. By taking the Fourier transform of the filter weights, it is possible to compute the response of the filter as a function of wavelength (Holloway, 1958). The wavelength response is shown in Figure 2 for the equivalent five-by-seventeen filter. Note that for the longest zonal harmonics the response is near unity, indicating that they are unaffected by the filtering. At a wavelength of three grid intervals, the zonal response is negative, indicating a 180 degree phase shift. The response, however, is only 10

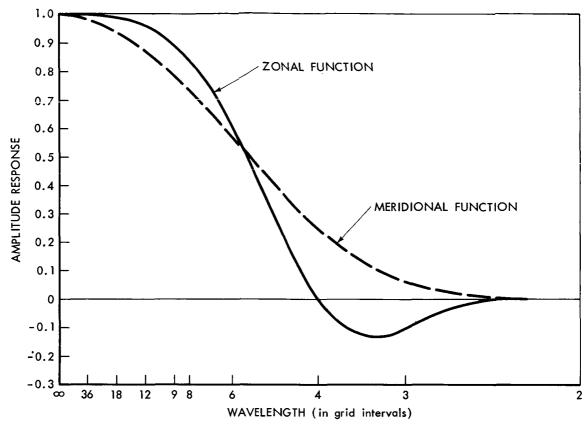


Figure 2. Amplitude Response of the Spatial Smoothing Operator in the Meridional and Zonal Directions as a Function of Wavelength

percent and disturbances at this wavelength were largely eliminated. Zonal disturbances at wavelengths of two and four grid intervals were eliminated completely.

After the smoothing operation, the data were analyzed by an electronic curve plotter at intervals of two degrees Kelvin. The resulting charts are presented in the next section.

5. TEN-DAY MEAN CHARTS

The TIROS VII 15 micron data have been compiled and mapped on a series of seventy-three ten-day mean charts, normally at five-day intervals, covering the 13-month period from launch (19 June 1963) to 16 July 1964. The charts are numbered such that in general a series of successive and contiguous ten-day charts (without time overlap) is made up of either the odd-numbered charts or the even-numbered charts. However, the phase of the two sets is staggered such that the beginning points in time of the maps of say the odd-numbered set occur at the midpoints in time of the maps of the even-numbered set or vice versa.

Because of occasional interrogation problems resulting in a failure to acquire the data successfully, the pattern of time-continuity is broken at several points in both sets of charts. The odd-numbered set is the more nearly continuous, suffering only one-to-three day breaks surrounding the five entries of "NO DATA ACQUIRED" in Table I, plus an eight-day break during the interval 5-12 May 1964. The even-numbered set suffers five extensive breaks in the intervals identified by entries of "NO DATA ACQUIRED" in Table I, plus a seven-day break during the interval 10-16 May 1964. Hence, though the final chart is numbered 78, there are five fewer actual charts represented because of the indicated intervals where no data were acquired. The degradation-corrected measurements on the charts are given in terms of equivalent blackbody temperatures (T_{BB}). All measurements were made in the nadir angle range 0° - 40°. Other pertinent data concerning the charts are documented in Table I.

ACKNOWLEDGMENTS

This project was conducted under the guidance and supervision of Mr. William R. Bandeen, Head of the Planetary Radiations Branch, Goddard Space Flight Center. The treatment of the vast amount of data was facilitated by Mr. Robert T. Hite, Head of the branch computing section, ably assisted by Mr. Gary Wolford and Mr. Walter Musial.

The efforts of these individuals are hereby gratefully acknowledged.

یب ا								$\overline{}$	_			_		_		T 1		_	1			-			T	$\overline{}$	_			_	_	_	-	- 7			_	$\neg op$	$\overline{}$
PAGE			20	51	25	53	54		22	26	29	28	29	09	61	62	63	64	65	99	29	89	69	2 5	7.5	: 2	74	75	94	77	48	64	80	81		82	83	84	82
22	þ		0.197	0.199	0.202	0.207	0.210		0.217	0.220	0.225	0.229	0.234	0.237	0.241	0.246	0.250	0.255	0.260	0.264	0.270	0.275	0.280	0.285	0.290	0.301	0.307	0.322	0.328	0.333	0,341	0.348	0.355	0.362		0.380	0.387	0.392	0.402
FACTOR	aţ		-43.0 0.197	-43.6	-44.2	-45.0	-45.6 0.210		-47.3 0.217	-48.2	-49.1	-50.1	-51.3	-52.0	-53.1	-54.2	-55.3	-56.5 0.255	-57.5	-58.6	-59.8	-61.2 0.275	-62.5	-63.8	0.69-	67.8	-69.2	-73.1	-74.5	-75.6	-77.5	-79.1	-80.9	-82.7 0.362		-86.8 0.380	-88.0 0.387	-90.0 0.392	-92.2 0.402
CORRECTION FACTORS (cf EQUATION 1)	ď,		-0.030	-0.031	-0.033	-0.034	-0.036		-0.035	-0.041	-0.043	-0.045	-0.047	-0.049	-0.051	-0.053	-0.055	-0.058	-0.060	-0.062	-0.065				-0.014		i	-0.087	-0.090	-0.092	i T	-0.098	-0.100	-0.102		-0.109	-		
90	9 M		15.1	15.4 -(16.0 -0	16.2 -(16.7 -(17.5 -(18.0	18.5 -0	19.0	19.5 -(20.0	20.4 -0	20.9	21.3 -(22.0 -(22.8 -(23.7 -0			25.2 -(25.6			28.7 -0	29.3 -0	29.8 -0		31.4 -(32.0 -0	32.4 -0		34.2 -0		35.2 -0	36.0 -0.116
TOTAL NC. OF	Щ.	ACQUIRED	52 1	48	46 1	61 1	66 1	QUIRED	63	62 1	67 1	63 1	49 1	38 2	43 2	53 2	55 2	63 2	64 2	63 2	72 2	$\neg \neg$	T		33 2 2	T		58 2	51 2	40 2		40 3	35 3	31 3	URED	23	Ţ	T	26 3
		A ACQ	055	110	187	261		AC	475	553	611	1684	757	830	888	196	033	107	165	238	326	384	457	516	663	734	805	266	070	143	216	589	361	447	A ACQ	609	683	740	813
ORBITS	(INCL.	NO DATA	526-536 2909-3055	2977-3110	3050-3187	3126-3261	3181-3314	DATA	555-564 3341-3475	3414-3553	3472-3611	3545-3684	3620-3757	3691-3830	3750-3888	3827-3961	3896-4033	3969-4107	4027-4165	4100-4238	4173-4326	4246-4384	4319-4457	626-635 4377-4516	4525-4661	4598-4734	4671-4805	4861-4997	4917-5070	4990-5143	5077-5216	5150-5289	5224-5361	687-696 5296-5447	NO DATA ACQUIRED	5479-5609	5544-5683	706-715 5605-5740	711-720 5678-5813
FWRT	EEL?	NO	9-536	531-540	536-545	541-550	545-554	NC	5-564	260-269	564-573	569-578	574-583	579-588	583-592	288-597	593-602		\vdash	\rightarrow	612-622		622-631	3-635	632-641				662-671	929-199	_	677-686	682-691	969-	S	901-109	702-711	3-715	1-720
	_						\neg				64 56				П	64 588		64 598	64 60;	T			\neg	_				64 658	64 662							П		ğ	1
DATES	ř.)		Jan 64	Jan 64	Jan (5 Jan (9 Jan (Feb 6	Feb 6	Feb 6	3 Feb	8 Feb	Mar (Mar (Mar	Mar	3 Mar	7 Mar	Apr (Apr 6	Apr 6	Apr 6	9 Apr	o Apr	May 6	May 6	2 May	7 May	Jun 6	Jun 6	Jun 64	Jun 64	Jun 6		Jul 64	Jul 64	Jul 64	Jul 64
Ya i	ž		2 Jan-11 Jan	6 Jan-15 Jan	11 Jan-20 Jan 64	16 Jan-25 Jan 64	20 Jan-29 Jan 64		31 Jan-9 Feb 64	5 Feb-14 Feb 64	9 Feb-18 Feb	14 Feb-23 Feb 64	19 Feb-28 Feb 64	24 Feb-4 Mar 64	28 Feb-8 Mar 64	4 Mar-13 Mar	9 Mar-18 Mar 64	14 Mar-23 Mar 64 598-607	18 Mar-27 Mar 64 602-611	23 Mar-1 Apr 64	28 Mar-6 Apr 64	1 Apr-10 Apr 64	Apr-15 Apr 64	10 Apr-19 Apr 64	16 Apr-25 Apr 64 20 Apr-29 Apr 64	25 Apr-4 May	30 Apr-9 May 64	13 May-22 May 64 658-667	May-27 May 64	21 May-1 Jun 64	27 May-6 Jun 64	1 Jun-11 Jun 64	6 Jun-15 Jun 64	Jun-21 Jun 64		24 Jun-2 Jul	Jun-7 Jul	2 Jul-11 Jul 64	7 Jul-16 Jul 64
- E		40	41 2	42 6	\dashv	44 16	45 20	46	47 31	48 5]	49 9 1	50 14	51 19	52 24	53 28	54 4 1	55 91	56 14	57 18	58 23	59 28	-+	-	+	54 15	+-	+-	67 13	17		\vdash	71 13	72 6 J	73 11	74	├ ┤	-	-+	78 7.3
CHART	ž	4	4	4	4	4		_	4	4	4		ري		2	2	2	2	2	2	2	9	"	9 (۳	9		9	9	9		7	2		_		_	7	_
PAGE	4	13	14	15	16	17	18	6	0	П	22	23	4	2	26	27	28	59	ಜ	_				[.	٦,	88	39		_	~	_	_				47	48		49
į a	-				7	1		19	20	21	2	2	24	25	2	2	~	2	ñ	31	32	33	34		3.7	\perp		I I			43	44	45		46	4		- 1	
	i P	0.098		0.115	0.118	0.120	_		Ц.	0.130	0.131	-		0.135		0.140			0.145	0.147	0.148	0.150	0.152	0.153	0.157	0.159	0.161	0.163	0.165	0.166		0.170	0.173			0.181	0.183	- 1	
	T	\vdash	-24.0 0.107	-26.0 0.115 1	0.118	-27.0 0.120 1	_	-28.2 0.128 1	-28.2 0.128 2	-28.6 0.130 2		-29.2 0.132 2	-29.5 0.134 2	-30.0 0.135 2	-30.1 0.137 2	-30.5 0.140 2	-30.8 0.141 2	-31.1 0.143 2	0.145	-32.0 0.147 3	0.148	0.150	_	0.153		0.159		I I	0.165		-36.7 0.168 4:				-39.0 0.178 4	Ш			-41.5 0.190
	T	-23.0 0.098	-24.0 0.107	-26.0 0.115	-26.2 0.118	-27.0 0.120	-27.5 0.125	-28.2 0.128	-28.2 0.128	-28.6 0.130	-29.0 0.131	-29.2 0.132	-29.5 0.134	-30.0 0.135	-30.1 0.137	-30.5 0.140	-30.8 0.141	-31.1 0.143	-31.5 0.145	-32.0 0.147	-32.1 0.148	-32.6 0.150	-33.0 0.152	-33.3 0.153	-34.0 0.157	-34.5 0.159	-34.9 0.161	-35.2 0.163	-35.9 0.165	-36.2 0.166	-36.7 0.168	-37.1 0.170	-37.7 0.173		-39.0 0.178	-39.5 0.181	-40.0 0.183		-41.5 0.190
CORRECTION FACTORS (cf EQUATION 1)	T	-0.047 -23.0 0.098	-0.042 -24.0 0.107	-0.033 -26.0 0.115	-0.025 -26.2 0.118	0.120	-27.5 0.125		Ц.	0.130	0.131	-		0.135	0.137	0.0 -30.5 0.140			0.145	0.0 -32.0 0.147	0.0 -32.1 0.148	-0.001 -32.6 0.150	-0.002 -33.0 0.152	-0.003 -33.3 0.153	0.157	-0.007 -34.5 0.159	0.161	0.163	-0.011 -35.9 0.165	-0.013 -36.2 0.166	-0.014 -36.7 0.168	-0.016 -37.1 0.170	-0.017 -37.7 0.173	Q	-0.021 -39.0 0.178	-0.022 -39.5 0.181	3.2 -0.023 -40.0 0.183		-41.5 0.190
CORRECTION FACTORS (cf EQUATION 1)	aw bw af bf	-23.0 0.098	-24.0 0.107	-26.0 0.115	9.4 -0.025 -26.2 0.118	-0.012 -27.0 0.120	5.4 0.0 -27.5 0.125	0.0 -28.2 0.128	0.0 -28.2 0.128	0.0 -28.6 0.130	0.0 -29.0 0.131	0.0 -29.2 0.132	0.0 -29.5 0.134	0.0 -30.0 0.135	0.0 -30.1 0.137	0.0 -30.5 0.140	0.0 -30.8 0.141	0.0 -31.1 0.143	0.0 -31.5 0.145	7.3 0.0 -32.0 0.147	7.6 0.0 -32.1 0.148	7.8 -0.001 -32.6 0.150	8.0 -0.002 -33.0 0.152	8.2 -0.003 -33.3 0.153	-0.004 -33.7 0.155	9.0 -0.007 -34.5 0.159	-0.009 -34.9 0.161	-0.010 -35.2 0.163	-35.9 0.165	-36.2 0.166	-36.7 0.168	-37.1 0.170	-37.7 0.173	QUIRED	-39.0 0.178	-39.5 0.181	3.2 -0.023 -40.0 0.183		
TOTAL CORRECTION FACTORS (cf EQUATION 1)	ORBITS aw bw af bf	36 56 13.2 -0.047 -23.0 0.098	55 12.4 -0.042 -24.0 0.107	47 10.8 -0.033 -26.0 0.115	60 9.4 -0.025 -26.2 0.118	64 7.8 -0.012 -27.0 0.120	67 5.4 0.0 -27.5 0.125	60 5.6 0.0 -28.2 0.128	62 5.6 0.0 -28.2 0.128	50 5.8 0.0 -28.6 0.130	46 5.9 0.0 -29.0 0.131	44 6.0 0.0 -29.2 0.132	52 6.0 0.0 -29.5 0.134	52 6.2 0.0 -30.0 0.135	59 6.4 0.0 -30.1 0.137	01 49 6.5 0.0 -30.5 0.140	60 53 6.7 0.0 -30.8 0.141	56 6.9 0.0 -31.1 0.143	52 7.1 0.0 -31.5 0.145	79 47 7.3 0.0 -32.0 0.147	52 7.6 0.0 -32.1 0.148	51 7.8 -0.001 -32.6 0.150	57 8.0 -0.002 -33.0 0.152	61 8.2 -0.003 -33.3 0.153	56 8.8 -0.006 -34.0 0.157	56 9.0 -0.007 -34.5 0.159	58 9.4 -0.009 -34.9 0.161	56 9.7 -0.010 -35.2 0.163	94 57 10.0 -0.011 -35.9 0.165	66 52 10.4 -0.013 -36.2 0.166	42 10.7 -0.014 -36.7 0.168	50 11.2 -0.016 -37.1 0.170	55 11.4 -0.017 -37.7 0.173	A ACQUIRED	37 12.5 -0.021 -39.0 0.178	43 12.9 -0.022 -39.5 0.181	06 48 13.2 -0.023 -40.0 0.183	CQURED	43 14.0 -0.026 -41.5 0.190
CORRECTION FACTORS (cf EQUATION 1)	ORBITS aw bw af bf	36 56 13.2 -0.047 -23.0 0.098	55 12.4 -0.042 -24.0 0.107	47 10.8 -0.033 -26.0 0.115	60 9.4 -0.025 -26.2 0.118	64 7.8 -0.012 -27.0 0.120	67 5.4 0.0 -27.5 0.125	60 5.6 0.0 -28.2 0.128	62 5.6 0.0 -28.2 0.128	50 5.8 0.0 -28.6 0.130	46 5.9 0.0 -29.0 0.131	44 6.0 0.0 -29.2 0.132	52 6.0 0.0 -29.5 0.134	52 6.2 0.0 -30.0 0.135	59 6.4 0.0 -30.1 0.137	01 49 6.5 0.0 -30.5 0.140	60 53 6.7 0.0 -30.8 0.141	56 6.9 0.0 -31.1 0.143	52 7.1 0.0 -31.5 0.145	79 47 7.3 0.0 -32.0 0.147	52 7.6 0.0 -32.1 0.148	51 7.8 -0.001 -32.6 0.150	57 8.0 -0.002 -33.0 0.152	61 8.2 -0.003 -33.3 0.153	56 8.8 -0.006 -34.0 0.157	56 9.0 -0.007 -34.5 0.159	58 9.4 -0.009 -34.9 0.161	56 9.7 -0.010 -35.2 0.163	94 57 10.0 -0.011 -35.9 0.165	66 52 10.4 -0.013 -36.2 0.166	42 10.7 -0.014 -36.7 0.168	50 11.2 -0.016 -37.1 0.170	55 11.4 -0.017 -37.7 0.173	•	37 12.5 -0.021 -39.0 0.178	43 12.9 -0.022 -39.5 0.181	06 48 13.2 -0.023 -40.0 0.183	CQURED	43 14.0 -0.026 -41.5 0.190
ORBITS TOTAL CORRECTION FACTORS (cf EQUATION 1)	(INCL.) ORBITS aw bw ar br	0001-0136 56 13.2 -0.047 -23.0 0.098	55 12.4 -0.042 -24.0 0.107	47 10.8 -0.033 -26.0 0.115	60 9.4 -0.025 -26.2 0.118	64 7.8 -0.012 -27.0 0.120	67 5.4 0.0 -27.5 0.125	60 5.6 0.0 -28.2 0.128	62 5.6 0.0 -28.2 0.128	50 5.8 0.0 -28.6 0.130	46 5.9 0.0 -29.0 0.131	44 6.0 0.0 -29.2 0.132	52 6.0 0.0 -29.5 0.134	52 6.2 0.0 -30.0 0.135	59 6.4 0.0 -30.1 0.137	01 49 6.5 0.0 -30.5 0.140	60 53 6.7 0.0 -30.8 0.141	56 6.9 0.0 -31.1 0.143	52 7.1 0.0 -31.5 0.145	79 47 7.3 0.0 -32.0 0.147	52 7.6 0.0 -32.1 0.148	51 7.8 -0.001 -32.6 0.150	57 8.0 -0.002 -33.0 0.152	61 8.2 -0.003 -33.3 0.153	56 8.8 -0.006 -34.0 0.157	56 9.0 -0.007 -34.5 0.159	58 9.4 -0.009 -34.9 0.161	56 9.7 -0.010 -35.2 0.163	94 57 10.0 -0.011 -35.9 0.165	66 52 10.4 -0.013 -36.2 0.166	42 10.7 -0.014 -36.7 0.168	2176-2312 50 11.2 -0.016 -37.1 0.170	55 11.4 -0.017 -37.7 0.173	NO DATA ACQUIRED	37 12.5 -0.021 -39.0 0.178	2512-2647 43 12.9 -0.022 -39.5 0.181	06 48 13.2 -0.023 -40.0 0.183	CQURED	43 14.0 -0.026 -41.5 0.190
TOTAL CORRECTION FACTORS (cf EQUATION 1)	(INCL.) ORBITS aw bw ar br	333-342 0001-0136 56 13.2 -0.047 -23.0 0.098	337-346 0058-0192 55 12.4 -0.042 -24.0 0.107	343-351 0146-0270 47 10.8 -0.033 -26.0 0.115	347-356 0205-0343 60 9.4 -0.025 -26.2 0.118	352-361 0277-0416 64 7.8 -0.012 -27.0 0.120	357-366 0350-0489 67 5.4 0.0 -27.5 0.125	362-370 0423-0547 60 5.6 0.0 -28.2 0.128	366-375 0481-0620 62 5.6 0.0 -28.2 0.128	371-380 0554-0692 50 5.8 0.0 -28.6 0.130	375-384 0613-0751 46 5.9 0.0 -29.0 0.131	381-389 0702-0821 44 6.0 0.0 -29.2 0.132	384-394 0744-0896 52 6.0 0.0 -29.5 0.134	390-399 0831-0970 52 6.2 0.0 -30.0 0.135	394-403 0890-1028 59 6.4 0.0 -30.1 0.137	400-408 0977-1101 49 6.5 0.0 -30.5 0.140	403-412 1021-1160 53 6.7 0.0 -30.8 0.141	409-418 1109-1246 56 6.9 0.0 -31.1 0.143	413-422 1167-1306 52 7.1 0.0 -31.5 0.145	419-427 1255-1379 47 7.3 0.0 -32.0 0.147	423-432 1313-1450 52 7.6 0.0 -32.1 0.148	428-437 1387-1525 51 7.8 -0.001 -32.6 0.150	433-442 1461-1597 57 8.0 -0.002 -33.0 0.152	437-446 1517-1655 61 8.2 -0.003 -33.3 0.153	447-456 1664-1801 56 8.8 -0.006 -34.0 0.157	452-461 1736-1875 56 9.0 -0.007 -34.5 0.159	456-465 1794-1933 58 9.4 -0.009 -34.9 0.161	461-470 1867-2006 56 9.7 -0.010 -35.2 0.163	466-475 1940-2094 57 10.0 -0.011 -35.9 0.165	471-480 2013-2166 52 10.4 -0.013 -36.2 0.166	475-484 2086-2225 42 10.7 -0.014 -36.7 0.168	481-490 2176-2312 50 11.2 -0.016 -37.1 0.170	485-495 2234-2379 55 11.4 -0.017 -37.7 0.173	•	496-505 2437-2575 37 12.5 -0.021 -39.0 0.178	501-510 2512-2647 43 12.9 -0.022 -39.5 0.181	505-514 2568-2706 48 13.2 -0.023 -40.0 0.183	CQURED	43 14.0 -0.026 -41.5 0.190
FMRT ORBITS TOTAL CORRECTION FACTORS	REELS (INCL.) ORBITS a, b, af bf	333-342 0001-0136 56 13.2 -0.047 -23.0 0.098	337-346 0058-0192 55 12.4 -0.042 -24.0 0.107	343-351 0146-0270 47 10.8 -0.033 -26.0 0.115	347-356 0205-0343 60 9.4 -0.025 -26.2 0.118	352-361 0277-0416 64 7.8 -0.012 -27.0 0.120	357-366 0350-0489 67 5.4 0.0 -27.5 0.125	362-370 0423-0547 60 5.6 0.0 -28.2 0.128	366-375 0481-0620 62 5.6 0.0 -28.2 0.128	371-380 0554-0692 50 5.8 0.0 -28.6 0.130	375-384 0613-0751 46 5.9 0.0 -29.0 0.131	381-389 0702-0821 44 6.0 0.0 -29.2 0.132	384-394 0744-0896 52 6.0 0.0 -29.5 0.134	390-399 0831-0970 52 6.2 0.0 -30.0 0.135	394-403 0890-1028 59 6.4 0.0 -30.1 0.137	400-408 0977-1101 49 6.5 0.0 -30.5 0.140	403-412 1021-1160 53 6.7 0.0 -30.8 0.141	409-418 1109-1246 56 6.9 0.0 -31.1 0.143	413-422 1167-1306 52 7.1 0.0 -31.5 0.145	419-427 1255-1379 47 7.3 0.0 -32.0 0.147	423-432 1313-1450 52 7.6 0.0 -32.1 0.148	428-437 1387-1525 51 7.8 -0.001 -32.6 0.150	433-442 1461-1597 57 8.0 -0.002 -33.0 0.152	437-446 1517-1655 61 8.2 -0.003 -33.3 0.153	447-456 1664-1801 56 8.8 -0.006 -34.0 0.157	452-461 1736-1875 56 9.0 -0.007 -34.5 0.159	456-465 1794-1933 58 9.4 -0.009 -34.9 0.161	461-470 1867-2006 56 9.7 -0.010 -35.2 0.163	466-475 1940-2094 57 10.0 -0.011 -35.9 0.165	471-480 2013-2166 52 10.4 -0.013 -36.2 0.166	475-484 2086-2225 42 10.7 -0.014 -36.7 0.168	481-490 2176-2312 50 11.2 -0.016 -37.1 0.170	485-495 2234-2379 55 11.4 -0.017 -37.7 0.173	•	496-505 2437-2575 37 12.5 -0.021 -39.0 0.178	501-510 2512-2647 43 12.9 -0.022 -39.5 0.181	505-514 2568-2706 48 13.2 -0.023 -40.0 0.183	CQURED	43 14.0 -0.026 -41.5 0.190
ORBITS TOTAL CORRECTION FACTORS (cf EQUATION 1)	REELS (INCL.) ORBITS a, b, af bf	333-342 0001-0136 56 13.2 -0.047 -23.0 0.098	337-346 0058-0192 55 12.4 -0.042 -24.0 0.107	343-351 0146-0270 47 10.8 -0.033 -26.0 0.115	347-356 0205-0343 60 9.4 -0.025 -26.2 0.118	352-361 0277-0416 64 7.8 -0.012 -27.0 0.120	357-366 0350-0489 67 5.4 0.0 -27.5 0.125	362-370 0423-0547 60 5.6 0.0 -28.2 0.128	366-375 0481-0620 62 5.6 0.0 -28.2 0.128	371-380 0554-0692 50 5.8 0.0 -28.6 0.130	375-384 0613-0751 46 5.9 0.0 -29.0 0.131	381-389 0702-0821 44 6.0 0.0 -29.2 0.132	384-394 0744-0896 52 6.0 0.0 -29.5 0.134	390-399 0831-0970 52 6.2 0.0 -30.0 0.135	394-403 0890-1028 59 6.4 0.0 -30.1 0.137	400-408 0977-1101 49 6.5 0.0 -30.5 0.140	403-412 1021-1160 53 6.7 0.0 -30.8 0.141	409-418 1109-1246 56 6.9 0.0 -31.1 0.143	413-422 1167-1306 52 7.1 0.0 -31.5 0.145	419-427 1255-1379 47 7.3 0.0 -32.0 0.147	423-432 1313-1450 52 7.6 0.0 -32.1 0.148	428-437 1387-1525 51 7.8 -0.001 -32.6 0.150	433-442 1461-1597 57 8.0 -0.002 -33.0 0.152	437-446 1517-1655 61 8.2 -0.003 -33.3 0.153	447-456 1664-1801 56 8.8 -0.006 -34.0 0.157	452-461 1736-1875 56 9.0 -0.007 -34.5 0.159	456-465 1794-1933 58 9.4 -0.009 -34.9 0.161	461-470 1867-2006 56 9.7 -0.010 -35.2 0.163	466-475 1940-2094 57 10.0 -0.011 -35.9 0.165	471-480 2013-2166 52 10.4 -0.013 -36.2 0.166	475-484 2086-2225 42 10.7 -0.014 -36.7 0.168	481-490 2176-2312 50 11.2 -0.016 -37.1 0.170	485-495 2234-2379 55 11.4 -0.017 -37.7 0.173	•	496-505 2437-2575 37 12.5 -0.021 -39.0 0.178	501-510 2512-2647 43 12.9 -0.022 -39.5 0.181	505-514 2568-2706 48 13.2 -0.023 -40.0 0.183	CQURED	43 14.0 -0.026 -41.5 0.190
FMRT ORBITS TOTAL CORRECTION FACTORS	(INCL.) REELS (INCL.) ORBITS aw bw af bf	0001-0136 56 13.2 -0.047 -23.0 0.098	55 12.4 -0.042 -24.0 0.107	47 10.8 -0.033 -26.0 0.115	347-356 0205-0343 60 9.4 -0.025 -26.2 0.118	352-361 0277-0416 64 7.8 -0.012 -27.0 0.120	357-366 0350-0489 67 5.4 0.0 -27.5 0.125	60 5.6 0.0 -28.2 0.128	62 5.6 0.0 -28.2 0.128	50 5.8 0.0 -28.6 0.130	375-384 0613-0751 46 5.9 0.0 -29.0 0.131	44 6.0 0.0 -29.2 0.132	52 6.0 0.0 -29.5 0.134	52 6.2 0.0 -30.0 0.135	3 394-403 0890-1028 59 6.4 0.0 -30.1 0.137	24 Aug-1 Sep 63 400-408 0977-1101 49 6.5 0.0 -30.5 0.140	403-412 1021-1160 53 6.7 0.0 -30.8 0.141	409-418 1109-1246 56 6.9 0.0 -31.1 0.143	6 Sep-15 Sep 63 413-422 1167-1306 52 7.1 0.0 -31.5 0.145	12 Sep-20 Sep 63 419-427 1255-1379 47 7.3 0.0 -32.0 0.147	16 Sep-25 Sep 63 423-432 1313-1450 52 7.6 0.0 -32.1 0.148	21 Sep-30 Sep 63 428-437 1387-1525 51 7.8 -0.001 -32.6 0.150	26 Sep-5 Oct 63 433-442 1461-1597 57 8.0 -0.002 -33.0 0.152	30 Sep-9 Oct 63 437-446 1517-1655 61 8.2 -0.003 -33.3 0.153	56 8.8 -0.006 -34.0 0.157	15 Oct-24 Oct 63 452-461 1736-1875 56 9.0 -0.007 -34.5 0.159	58 9.4 -0.009 -34.9 0.161	24 Oct-2 Nov 63 461-470 1867-2006 56 9.7 -0.010 -35.2 0.163	29 Oct-7 Nov 63 466-475 1940-2094 57 10.0 -0.011 -35.9 0.165	3 Nov-12 Nov 63 471-480 2013-2166 52 10.4 -0.013 -36.2 0.166	7 Nov-16 Nov 63 475-484 2086-2225 42 10.7 -0.014 -36.7 0.168	13 Nov-22 Nov 63 481-490 2176-2312 50 11.2 -0.016 -37.1 0.170	55 11.4 -0.017 -37.7 0.173	•	1 Dec-10 Dec 63 496-505 2437-2575 37 12.5 -0.021 -39.0 0.178	6 Dec-15 Dec 63 501-510 2512-2647 43 12.9 -0.022 -39.5 0.181	10 Dec-19 Dec 63 505-514 2568-2706 48 13.2 -0.023 -40.0 0.183	NO DATA ACQUIRED	14.0 -0.026 -41.5 0.190

REFERENCES

- Allison, L. J., and G. Warnecke, 1964: "Examples of Certain Data Reduction and Mapping Procedures Utilizing TIROS III Five-Channel Radiometer Data". Goddard Space Flight Center Document X-651-64-132, 30 April 1964, 38 pp.
- Bandeen, W. R., B. J. Conrath and R. A. Hanel, 1963: Experimental confirmation from the TIROS VII meteorological satellite of the theoretically calculated radiance of the earth within the 15-micron band of carbon dioxide, J. A. S., 20, 609-614.
- Boville, B. W., 1960: The Aleution Stratospheric Anticyclone. Jn. Met, $\underline{17}$, 329-336.
- Holloway, J. L., 1958: Smoothing and filtering of time series and space fields, Adv. in Geophysics, 4, 351-389.
- Kunde, V. G., 1966: unpublished personal communication.
- Nordberg, W., W. R. Bandeen, G. Warnecke, and V. G. Kunde, 1965: Stratospheric temperature patterns based on radiometric measurements from the TIROS VII satellite. pp. 782-809 in <u>Space Research V. Ed. by P. Muller</u>, North-Holland Publishing Company, Amsterdam.
- Staff Members, 1964: TIROS VII Radiation Data Catalog and Users' Manual, Vol. 1, Goddard Space Flight Center, Greenbelt, Maryland, 30 September 1964, 256 pp.
- Staff Members, 1965: TIROS VII Radiation Data Catalog and Users' Manual, Vol. 3, Goddard Space Flight Center, Greenbelt, Maryland, 15 October 1965, 269 pp.
- Starr, V. P. and M. Wallace, 1964: Mechanics of eddy processes in the tropical troposphere, Pure and Applied Geophysics, <u>58</u>, 138-144.
- Teweles, S., 1963: Spectral Aspects of the Stratospheric Circulation During the IGY. Planetary Circ Proj Rpt No. 8, Meteor. Dept., Mass. Inst. of Tech., 191 pp.
- Wallington, C. E., 1962: The use of smoothing or filtering operators in numerical forecasting. Q.J.R.M.S., <u>88</u>, 470-484.

